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### $T_1$ Measurements incorporating flip angle calibration and correction in vivo

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### Abstract

In this work, we propose a variable FA method that combines *in vivo* flip angle (FA) calibration and correction with a short TR variable FA approach for a fast and accurate  $T_1$  mapping. The precision  $T_1$ s measured across a uniform milk phantom is estimated to be 2.65% using the conventional (slow) inversion recovery (IR) method and 28.5% for the variable FA method without FA correction, and 2.2% when FA correction is included. These results demonstrate that the sensitivity of the variable FA method to RF nonuniformities can be dramatically reduced when these nonuniformities are directly measured and corrected. The acquisition time for this approach decreases to 10 min from 85 min for the conventional IR method. In addition, we report that the averaged  $T_1$ s measured from five normal subjects are  $900 \pm 3$  ms,  $1337 \pm 8$  ms and  $2180 \pm 25$  ms in white matter (WM), gray matter (GM) and cerebral spinal fluid (CSF) using the variable flip angle method with FA correction at 3 T, respectively. These results are consistent with previously reported values obtained with much longer acquisition times. The method reduces the total scan time for whole brain  $T_1$  mapping, including FA measurement and calibration, to approximately 6 min. The novelty of this method lies in the *in vivo* calibration and the correction of the FAs, thereby allowing a rapid and accurate  $T_1$  mapping at high field for many applications.

Keywords: RF inhomogeneity; RF calibration; Spin-lattice relaxation time; SSGE

### 1. Introduction

The spin-lattice relaxation time,  $T_1$ , varies between different tissues and pathologies, and therefore has been exploited as a contrast mechanism in MR imaging [1]. There has been strong interest in rapid and accurate  $T_1$ measurements, which are essential for many research and clinic applications [2–4], such as spin labeling techniques [5] and dynamic contrast agent studies [6]. Conventionally,  $T_1$  can be estimated using saturation-recovery (SR) sequences with multiple repetition times (TRs), or using inversion recovery (IR) sequences with multiple inversion

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times (TIs). However, these conventional sequences require long acquisition times in order to measure the longitudinal magnetization at the multiple time points needed for accurate  $T_1$  measurements (typically with a resolution of 256 × 256, and 4-8 sampling points). To accelerate data acquisition, several approaches have been proposed. Look and Locker used a series of limited FA pulses to sample the  $T_1$  recovery curve following a single inversion pulse [7]. Fast low angle shot (FLASH) sequences have also been employed with very short TR to rapidly acquire images for  $T_1$  mapping [8,9]. However, these methods suffer from poor SNR due to the use of small flip angles. Although echo planar imaging (EPI) allows extremely fast image acquisitions with high SNR [10,11], the low spatial resolution and high sensitivity to magnetic field inhomogeneities limit its applicability. To overcome these shortages, a

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variable FA method, originally introduced in 1974 [12] and investigated by a number of authors [13–15], is used to estimate  $T_1$  with an accuracy and a precision similar to that achieved by the IR and SR techniques, but with a significant reduction in acquisition time. However, since FAs vary spatially across an image due to RF/tissue interactions and/or from nonideal slice profiles, these variations in the FAs lead to errors in the measured  $T_1$ , particularly with the variable FA method. With a variable FA method, Luzikov et al. reported 15% errors in  $T_1$  measurements with 10% errors in FAs [16,17], and Clare et al. [18] found 20% deviations in  $T_1$  in a uniform phantom at 3 T. Therefore, it is critical to compensate imperfections in FA distribution when the variable FA method is used at high field (>1.5 T) [19].

In this work, we present a method for rapid and accurate  $T_1$  mapping. Absolute FAs are obtained for each voxel through *in vivo* measurement of relative FAs and an FA calibration factor. Phantom and *in vivo* studies indicate that the precision and the accuracy of the  $T_1$ s measured by this method are comparable to those estimated using conventional IR-gradient echo (GE) sequences requiring much longer acquisition times.

### 2. Theory

### 2.1. Measurement of FA in vivo

For GE sequences, if TR is much longer than  $T_1$  (TR > 5 $T_1$ ) and  $T_2$  (TR > 5 $T_2$ ) of a sample, the signal intensity *SI*(*x*) is given by [16,20,21],

$$SI(x) = C(x) \cdot S(x) \cdot \sin \alpha(x), \tag{1}$$

where  $\alpha(x)$ , SI(x) and S(x) are the excitation FA, the signal intensity, and the reception sensitivity at the position x in an image, respectively. The variable, C(x), is dependent upon tissue properties (proton density, and  $T_2^*$ ) and image acquisition parameters, such as echo time (TE) and TR. The ratio of signal intensities SI<sub> $\alpha_1$ </sub>(x)/SI<sub> $\alpha_2$ </sub>(x)of the two GE images at different nominal FAs  $\alpha_1$  and  $\alpha_2$  is given by

$$\lambda(x) = \frac{\mathbf{SI}_{\alpha_2}(x)}{\mathbf{SI}_{\alpha_1}(x)} = \sin \alpha_2(x) / \sin \alpha_1(x).$$
<sup>(2)</sup>

Note that Eq. (2) also assumes that the slice excitation profile for  $\alpha_1$  is identical to that for  $\alpha_2$ . Based on this assumption, it is theoretically possible to estimate the actual value corresponding to  $\alpha_1$  at each voxel in a sample (denoted  $\alpha_{1,\text{meas}}(x)$ ) as previously described [16]. That is,

$$\alpha_{1,\text{meas}}(x) = \arccos\left(\lambda(x)/2\right),\tag{3}$$

where  $\alpha_2 = 2\alpha_1$  is assumed. Once this calibration process has been accomplished, the actual FA across the sample can be determined for any subsequent experiment (denoted  $\alpha_{absolute}(x)$ ) for which a nominal FA  $\alpha_{nom}$  is specified. This is given by:

$$\alpha_{\text{absolute}}(x) = k \cdot (\alpha_{1,\text{meas}}(x)/\alpha_1) \cdot \alpha_{\text{nom}}, \qquad (4)$$

where k is a sample-specific FA calibration factor relating the input RF power to the actual FAs achieved. It is strongly dependent upon the electromagnetic properties of the sample and the relative position between the coil and the sample. The k factor is crucial to obtain absolute FA values as FA mapping generally only provides relative FA maps without calibration. The nominal FA is chiefly determined by the amplitude and duration of the applied RF pulse, however, the coupling between the RF coil and the sample can alter the flip angle achieved. Consequently, it is necessary to recalibrate the RF transmitter for each image acquisition in vivo if quantitative data are to be obtained. It is noted that the  $\alpha_1$  in Eq. (2) is the nominal FA used for determining  $\alpha_{meas}(x)$  and the absolute FA  $(\alpha_{absolute})$  corresponding to a nominal FA,  $\alpha_{nom}$ , is calculated based on a linear relationship between the measured FA and the nominal FA.

If the FAs across a sample are uniform, k can be estimated using a free-induction decay (FID) experiment with different FAs. The actual FA of 90° yields the maximum signal intensity and the actual FA of 180° produces the null signal intensity for an FID at a long TR [24]. RF nonuniformities, however, negatively impact the use of such standard 90° and 180° methods (which do not take spatial variations into account) for estimating k. Other methods have been reported to estimate k taking into account spatial variations in flip angle with the penalty of additional scan time [25,26]. Here, we propose a method in which kis determined by the slope of the measured FA versus the nominal FA curve. The measured FA at each voxel is then scaled accordingly.

# 2.2. Measurement of $T_1$ using variable FA with RF correction terms

When the transverse magnetization dephases between successive RF excitation pulses within a TR, the signal intensity for an ideal steady-state gradient-echo (SSGE) sequence with an excitation FA of  $\alpha$  can be approximated as [22]:

$$\mathbf{SI}(\alpha(x)) = M_0(x) \cdot \sin \alpha(x) \cdot \frac{(1 - E_1(x))}{1 - E_1(x) \cdot \cos \alpha(x)} \cdot S(x), \quad (5)$$

where  $E_1(x) = \exp(-\text{TR}/T_1(x))$ .  $M_0(x)$  and S(x) are the equilibrium longitudinal magnetization and the receive sensitivity at the location x, respectively. In practice, the RF coil configuration, the interaction between a coil and a subject, and an imperfect slice profile produces variable FAs, such that the actual FA,  $\alpha_{\text{absolute}}(x)$ , is a function of spatial location. Thus, Eq. (5) must be modified as [23]:

$$\frac{\mathrm{SI}_{\mathrm{measured}}(x)}{\sin(\alpha_{\mathrm{absolute}}(x))} = \frac{\mathrm{SI}_{\mathrm{measured}}(x)}{\tan(\alpha_{\mathrm{absolute}}(x))} \cdot E_1(x) + M_0(x) \cdot S(x)$$
$$\cdot (1 - E_1(x)), \tag{6}$$

Finally,  $T_1$  can be expressed as [15]:

$$T_1(x) = -\mathbf{T}\mathbf{R}/\ln(E_1(x)). \tag{7}$$

Since the slope,  $E_1$ , depends only on a known TR and the unknown  $T_1$ , the  $T_1$  will be independent of proton density, reception sensitivity, and  $T_2^*$ . Thus, the  $T_1$  is calculated from the expression: SI<sub>measured</sub>(x)/sin $\alpha_{absolute}(x)$  vs. SI<sub>measured</sub>(x)/tan $\alpha_{absolute}(x)$ .

### 2.3. Optimizing the $T_1$ acquisition

Many authors have investigated the optimum parameters for measuring  $T_1$  at a fixed TR with a variable FA method [2,13,15]. For quantitative comparisons, we define a normalized dynamic range (DR) of regression as:

DR 
$$\propto \frac{1}{1 - E_1 \cos(\alpha_{1,\text{nom}})} - \frac{1}{1 - E_1 \cos(\alpha_{2,\text{nom}})},$$
 (8)

where  $\alpha_{1,\text{nom}}$  and  $\alpha_{2,\text{nom}}$  are the two nominal FAs used to estimate  $T_1$ . Using Eq. (8), we can numerically calculate the DR at different FAs in the two FAs and the results are shown in Fig. 1 for a  $T_1$  of 1100 ms (the average  $T_1$ of GM and WM at 3 T) and a TR of 500 ms. Evaluation of the DR and SNR over all possible combinations of FAs yields optimal FAs of 23° and 122° to minimize the error of  $T_1$  measurement. This example also illustrates that the optimal FAs for  $T_1$  measurements are a function of both the tissue  $T_1$  and the TR.

## 2.4. Quantification of the linear relationship of the measured FA and nominal FA

To examine the range in which the linear relationship between the measured FA and the nominal FA holds, a normalized difference score parameter,  $\psi$ , can be defined as:

$$\psi(\alpha) = 2 * \frac{\mathrm{SI}_{\mathrm{simulated}}(\alpha) - \mathrm{SI}_{\mathrm{measured}}(\alpha)}{\mathrm{SI}_{\mathrm{simulated}}(\alpha) + \mathrm{SI}_{\mathrm{measured}}(\alpha)} * 100\%, \tag{9}$$

where SI<sub>simulated</sub>( $\alpha$ ) is the signal intensity of the image simulated according to Eq. (1) at the FA of  $\alpha$ . The  $\alpha$  is determined by the measured FA map using Eq. (4), based on the linear relationship. SI<sub>measured</sub>( $\alpha$ ) represents the signal intensity of the measured image at the FA of  $\alpha$ . Small  $\psi(\alpha)$  indicates that there is a good agreement between the measured FA and the nominal FA.

### 3. Methods

Five normal male adults with no history or physical findings of neurological diseases were studied. The mean age of the subjects was 37, (range from 25 to 45). The human study protocol was approved by the Institutional Review Board (IRB) at Yale University School of Medicine.

All phantoms and human brain images were acquired on a Siemens 3 T Trio system. Two cylindrical phantoms (15 cm in diameter) were used to evaluate the performance of the variable flip angle method with FA correction. One phantom was filled with 1% low fat milk (Deerfield farms) and the other was filled with oil. To examine the linear relationship between measured FAs and nominal FAs, measured FAs were obtained from both phantoms using a gradient echo sequence with  $\alpha_1$ s varying from 20° to 180° in increments of 10°, and  $\alpha_2$  varying from 40° to 360° with increments of 20°. The signal intensity of the images with different FAs was simulated according to Eq. (1), assuming that C(x) was constant for the homogeneous phantoms. S(x) was calculated according to ref [20]. The actual FA map for each nominal FA was estimated from Eq. (4), based on the relative FAs and k which were calculated using the images acquired at the FAs of 30, 60, and 120°.

A conventional IR gradient echo pulse sequence (TI = 300, 600, 1000, 1500, 2000 ms) with nonslice selective



Fig. 1. The dynamic range DR as a function of the prescribed flip angle  $\alpha_1$  and  $\alpha_2$  at a TR = 500 ms with  $T_1 = 1100$  ms. The optimum flip angles for minimizing the standard deviation of the  $T_1$  are 23° and 122°.

IR magnetization preparation was used for  $T_1$  mapping of the milk phantom and this  $T_1$  was used as a reference. The total acquisition time was approximately 85 min. The measured FA map of the milk phantom was obtained using a segmented-EPI sequence with excitation FAs of  $30^{\circ}$ .  $60^{\circ}$ . and 120°, respectively. The EPI segmentation factor was 7. Other acquisition parameters for the gradient echo IR method were TR/TE 8000/4 ms, FOV  $200 \times 200$  mm<sup>2</sup>, matrix  $128 \times 128$ , and slice thickness of 5 mm. The  $T_1$ s of the phantom were estimated using a nonlinear threeparameter fitting from the images acquired with the IR gradient echo sequence at different TIs. For the variable FA method with FA correction, the two images were acquired using multi-slice gradient echo sequence at the FAs of 23° and 122°, TR/TE 150/4 ms. Other parameters were the same as those in the IR method.

The term "slice profile" refers to the magnitude component of transverse magnetization as a function of location along the slice select direction, which is typically a nonlinear profile of FAs described by the Bloch equations. The slice profile is closely related to RF pulses and the applied slice selection gradients. A spherical phantom (17 cm diameter) filled with distilled water and NiSO<sub>4</sub>·H<sub>2</sub>O (1.25 g/l), was used to quantitatively evaluate the effect of the RF pulse profile on the measured FA. Two multi-slice axial images were acquired from the spherical phantom using conventional gradient echo at FAs of 45° and 90° to evaluate the effect of RF pulse profile. These images were acquired with TR/TE 2500/4 ms, FOV  $200 \times 200 \text{ mm}^2$ , matrix  $128 \times 128$ , slice thickness of 5 mm using three different RF excitation pulses (sinc, truncated sinc and Gaussian envelope profiles), with a 20 slice acquisition. The duration/bandwidth of the sinc, the truncated-sinc and the Gaussian RF pulses were 2.000/13.5, 5.120/20, and 5.120/ 10 ms/kHz, respectively. The measured relative FAs were calculated using Eq. (3) for these RF pulses. The calibration factor k for each RF pulse was determined from the slope of the measured FA vs. the nominal FA curves. After RF calibration, the absolute FA across the phantom was estimated according to Eq. (4). The  $T_1$  map was then derived from Eqs. (6) and (7).

For the in vivo studies, the FA maps were acquired using a segmented spin echo EPI sequence with nominal excitation FAs of 30, 60 and 120°, with TR/TE of 2500/4 ms, FOV  $240 \times 192$  mm<sup>2</sup>, matrix  $128 \times 102$ , slice thickness of 6 mm, bandwidth 752 Hz per pixel, an EPI segment factor of 7, and a total acquisition time of 37 seconds for each acquisition. The effect of using a TR that did not satisfy the condition  $TR \gg T_1$ , was also examined with a TR of 1740 ms which was only about 1.5 times the average  $T_1$  of GM and WM at 3.0 T. Since the measured FA map obtained at TR = 1740 ms did not significantly differ from that obtained at TR = 9000 ms [20], we concluded that the TR of 1740 ms could be used for FA mapping in GM and WM. The calibration of the FAs for human subjects was made assuming a linear relationship between the measured and nominal FAs. An in vivo calibration factor was calculated from the slope of the plot of the measured FA versus the nominal FA (measured from the  $30^{\circ}/60^{\circ}$  acquisitions) for each subject. Finally,  $T_1$ maps were estimated using the two gradient echo images with the nominal FAs of 23 and 122°, and short TR. Other acquisition parameters were: FOV  $240 \times 192 \text{ mm}^2$ , matrix  $256 \times 204$ , slice thickness 3 mm, TR/TE 500/4 ms, 40 slices, and a bandwidth of 360 Hz per pixel. The in vivo images were processed with the following steps: (1) lowintensity background noise, skull and extra-cranial tissues were all set to zero; (2) the images obtained in different acquisitions were registered to reduce the influence of misregistration/motion on the measured  $T_1$  [27]; (3) the  $T_1$  of each voxel was estimated. Since the  $T_1$  of each brain tissue is usually not reflected by a single value but by a distribution of values [28], histograms of the measured  $T_1$ s were fit using three Gaussian distributions representing the three main tissues: CSF, GM, and WM. The  $T_1$  of each tissue is then expressed as the mean of its Gaussian distribution.

### 4. Results

The measured versus the nominal FAs curves for the oil and milk phantoms are shown in Fig. 2a and b, respectively. The standard deviation (SD) of the measured FA is estimated for the whole FOV. The result shows that the linear relationship holds for both phantoms when the measured FA is less than 120°. Since the measured FA at 120° is actually calculated from images obtained at nominal FAs of  $\alpha_1 = 120^\circ$  and  $\alpha_2 = 240^\circ$ , this result indicates that the apparent nonlinearity of the measured FA above 120° is due to the nonlinearity of  $\alpha_2$  when  $\alpha_2$  is greater than 240°. The measured FAs in the milk phantom show greater nonuniformities compared to those measured with the oil phantom, as indicated by the larger error bars particularly at higher FAs.

The simulated images with actual FAs and receive sensitivity are shown in Fig. 3a for the oil phantom, and Fig. 3c for the phantom containing milk. The corresponding, experimentally measured images are displayed in Fig. 3b (oil), and Fig. 3d (milk). For the oil phantom, the simulated image is similar to the measured image even at the nominal FA of 240°, suggesting the linear relationship holds over this range. For the milk phantom, however, the image is significantly different from the measured image at that nominal FA.

Fig. 4 shows the normalized difference score,  $\psi$ , between the simulated and the measured images for the oil and milk phantoms shown in Fig. 3. In Fig. 4a (oil),  $\psi$  is less than 5%, and the simulated images are in good agreement with the measured images. In Fig. 4b (milk) the images are also in good agreement except over the range of  $160^{\circ} < \alpha < 240^{\circ}$ , where  $\psi$  is more than 5%. The discrepancy is primarily due to the low SNR in this FA range. Here the  $\psi$  value of 5% reflects a "transition point" from linear to nonlinear behavior.



Fig. 2. Plots showing the linear relationship between the measured flip angle and the prescribed nominal flip angle for phantoms containing oil (a) and milk (b).



Fig. 3. Simulated images rows (a and c), assuming a linear relationship between the prescribed flip angle and the nominal flip angle, and the measured images, rows (b and d), for the phantom containing oil (a and b) and milk (c and d) at different flip angles.

Moreover, FA calibration factors, ks, in Eq. (4) are easily estimated from the slopes of the averaged measured FA vs. the nominal FA curves of the phantoms shown in Fig. 2a and b, respectively. The slopes are 0.82 and 0.78 for the oil and milk phantoms, respectively, at nominal FAs lower than 120°. The normalized difference scores also support this calculation. For the oil phantom, the maximum peak in the difference score shown in Fig. 4a occurs at a FA of ~220°, which is in contrast to the theoretically predicted value of 180°; the standard nulling point. The ratio, 180/220°, is 0.82 which is identical to the slope calculated from Fig. 2. For the milk phantom, the FA exhibits sufficient RF inhomogeneity from the RF wave behavior such that the normalized difference score cannot provide this ratio. The difference in the k factors between the milk and oil phantoms emphasizes that k must be estimated for each sample, because the RF field response is sample dependent.

Fig. 5 displays the measured FA maps for (a) Gaussian, (b) sinc, and (c) truncated-sinc, RF pulses. The magnitude of the measured FA is normalized to a nominal FA of 45°. For each of these RF pulses, the largest FA (or strongest RF field) occurs at the center of the phantom in Fig. 5. The FA is largest for the sinc RF pulse, and smallest for the Gaussian RF pulse. The maximum differences in the measured FA maps between these pulses are larger than the standard deviation of the measured FA (which is approximately 2%), suggesting that RF pulse profiles influence the measured FA maps and subsequent  $T_1$  measurements. Even for RF pulses in the same category (sinc and



Fig. 4. The normalized difference score between the simulated images and the measured images for different flip angles for the phantom containing oil (a) and milk (b).



Fig. 5. The measured flip angle map for different RF pulses: Gaussian (a), sinc (b), and truncated sinc (c) at a nominal flip angle of 60°.

truncated-sinc), the truncated pulse design leads to a different pulse profile, which in turn leads to a different distribution of the measured FA map as shown in Fig. 5b and c. The results demonstrate that the variable flip angle approach with FA correction is sensitive to the slice profile, and that the influence of the slice profile on the measured  $T_1$  is accounted for with the FA mapping and calibration.

Fig. 6a shows the measured FA map of a milk phantom using a segmented-EPI sequence at the nominal FAs of 30°, 60°, and 120°. The measured FA map, calculated according to Eq. (4), demonstrates significant nonuniformities. The standard deviation of the measured FA over the entire phantom is 19% of the mean. The  $T_1$  images of the phantom, estimated from the two acquisitions at FAs of 23° and 122°, with the variable flip angle method with, and without FA correction, are shown in Fig. 6b and c, respectively. With the variable FA method, the  $T_1$  is  $1190 \pm 340$  ms, with the standard deviation approximately 28.5% of the mean  $T_1$ . With flip angle correction, the average  $T_1$  is 1493  $\pm$  33 ms, with the standard deviation reduced to only 2.2% of the mean. Using a gradient echo IR method with different TIs and an overall acquisition time of approximately 85 min, the  $T_1$  image calculated with

a three parameter nonlinear fitting routine is shown in Fig. 6d. The  $T_1$  is 1391  $\pm$  37 ms with the standard deviation representing only 2.6% of the mean.

The average k of the five subjects is 0.74, suggesting that a measured FA is generally smaller than the nominal FA *in vivo*. A representative FA map is shown in the top row of Fig. 7. In the FA map, the standard deviation across the slice is approximately 20% of the mean measured FA. With the variable FA method, the error in the measured FA propagates to the measured  $T_1$ . Thus, the  $T_1$  of GM in certain regions is comparable to that of the WM, as shown in the middle row of Fig. 7. Using the variable flip angle approach with FA correction, the error in the measured  $T_1$  is significantly reduced to around 2%. Thus, the  $T_1$  of GM and WM exhibits excellent contrast, as shown in Fig. 7 (bottom row). Across the 5 subjects, the average  $T_1$ s is: 900 ± 3 ms for WM, 1337 ± 8 ms for GM and 2180 ± 25 ms for CSF.

#### 5. Discussion

As field strength increases,  $T_1$  becomes longer and the constraint,  $TR > 5T_1$ , for conventional  $T_1$  mapping leads



Fig. 6. A flip angle map (a) at a nominal flip angle of 45°, and the corresponding  $T_1$  map before (b) and after (c) correction of RF non-uniformity based on the flip angle map for the phantom containing milk with the variable FA method, and the T1 map measured by conventional inversion recovery (d).



Fig. 7. The *in vivo* measured FA map (row a), and  $T_1$  maps obtained using the variable flip angle approach before (row b), and after (row c), *in vivo* flip angle mapping, calibration, and correction of the flip angle non-uniformity.

to prohibitively long acquisition times. Short TR gradient echo imaging with a variable FA method provides a means for rapid  $T_1$  mapping but is highly sensitive to RF inhomogeneity. Ropele et al. [29], previously showed that large errors in  $T_1$  mapping arose from variations in the measured FA caused by RF inhomogeneities or by nonideal slice profiles. By implementing the variable FA method, Wang et al. found a 10% standard deviation for  $T_1 = 1000$  ms at 1.5 T [13]. Mintzopoulos et al. [30], showed that errors in  $T_1$  of as much as 17% were obtained at 3 T, and the data presented above showed a 29% standard deviation for a phantom containing milk (Fig. 6b). These results demonstrate that with the variable FA method RF nonuniformities lead to significant errors in the measured  $T_1$ . Thus, it is necessary to correct for these effects. Venkatesan et al. [24] proposed an RF correction scheme that was only valid at low field where the transmission field and the reception sensitivity may be assumed to be identical [31]. Parker et al. [32], proposed a method to correct the effect of RF inhomogeneities on the measured  $T_1$  at 1.5 T. Both Venkatesan and Parker assumed that the transmission field and the reception sensitivity in a phantom were identical to those in a human brain at 1.5 T. However, neither of these assumptions is valid at high field. Our experimental results demonstrated that both the measured FA and the FA calibration factor were sample-dependent, and thus should be specifically measured for each sample. The strength of the variable flip angle approach with FA correction that we present here, is that the correction is tailored to the sample being imaged.

Generally, the relative FA map determines the precision or the error in the measured  $T_1$ . The accuracy of the measured  $T_1$  is determined by the absolute FA, which includes both the relative FA and the FA calibration factor. There is no gold standard for validating *in vivo* human brain  $T_1$ measurements. Such an evaluation is difficult due to many factors that can influence the  $T_1$ , such as temperature, partial volume effects, radiation damping, chemical exchange and perfusion. In this work, the  $T_1$ s reported by the other authors can be used to evaluate our proposed approach. Kim et al. [33], obtained a  $T_1$  of 939 for WM and 1354 ms for GM at 4 T. Wansapura et al. [34] reported a  $T_1$  of 832 ms for WM and 1331 for GM at 3 T. With our proposed approach, the average  $T_1$  in five subjects was  $900 \pm 3$  ms for WM, and  $1337 \pm 8$  ms for GM. The  $T_1$ s for WM and GM were 7.5% and 0.4% higher, respectively, than those obtained with Wansapura's method. Such discrepancy might arise from the fact that their  $T_1$  values were measured in a specific region of interest (ROI), while our  $T_1$ s were obtained from all of the tissue via fitting three Gaussian curves to the whole brain histogram. Partial volume effects could have affected the accuracy of the ROI method but should not influence the histogram fitting [28], possibly accounting for the difference in these values. With our proposed approach, the in vivo FA maps were measured at TR = 2500 ms which was shorter than  $T_1$  of CSF at 3 T. Errors in the FA estimation for voxels including CSF may have led to an underestimation of the  $T_1$  in CSF. Moreover, the FAs of 23 and 122° for estimating the  $T_1$  in vivo were optimal only for GM and WM at 3 T. Thus, there was larger error in the measured  $T_1$  of CSF.

Since scan time strongly influences the SNR of the images used for  $T_1$  calculations, an efficiency term can be defined to assess the effect of SNR on  $T_1$  as

$$\eta = \frac{T_1}{\sigma_{T_1} \cdot \sqrt{T_{\text{total}}}} \tag{10}$$

where  $\sigma_{T_1}$  is the standard deviation of a measured  $T_1$ , and  $T_{\text{total}}$  represents the total scan time for estimating the measured  $T_1$ . Crawley and Henkelman [35], showed maximum

 $\eta$  could be achieved by sampling just five TI points along the recovery curve at TR =  $3T_1$  using an IR method, compared to the methods of snapshot flash, Look–Locker, and accelerated Look–Locker. In this work, the  $\eta$  of the optimal IR method, is compared with the variable FA method with and without RF correction. The acquisition time for FA mapping is also included in the total acquisition time for our approach.

At the same spatial resolution, the efficiency  $\eta$ , is improved from 0.14 s<sup>1/2</sup> with the variable FA method to 1.9 s<sup>1/2</sup> when RF correction is included, while an  $\eta$  of 0.52 s<sup>1/2</sup> is obtained with the optimized IR method. These results indicate that the variable flip angle approach is not only rapid, but also has high  $\eta$  for estimating  $T_1$  mapping, compared to the other methods. It is also noted that the  $\eta$  for the variable FA approach without correction is lower than that of the optimized IR method at 3 T emphasizing the need for FA correction and calibration at high field strength.

The sources of error in the  $T_1$  measurements obtained with our method arise from several factors including, thermal noise, misregistration either between the actual FA map and the  $T_1$  acquisitions, or between different FA acquisitions alone, and off-resonance effects [36]. Tissue  $T_1$  may also vary with RF pulse-induced temperature changes, and other factors such as blood flow, chemical exchange as well as magnetic susceptibility.

The approach presented here has several advantages and disadvantages over the conventional IR method in  $T_1$  measurement, particularly at high field strength. (1) Human tissue  $T_1$  increases with the increasing static magnetic field, thus requiring increased scan time for estimating  $T_1$  with conventional IR method. For the variable flip angle approach incorporating RF correction, longer  $T_1$ s have little influence on the scan time. (2) The variable flip angle approach substantially shortens the scan time and thus is highly efficient with an approximately unchangeable precision. (3) The specific absorption rate (SAR) becomes a limiting factor for some sequences at high field and the elimination of multiple IR pulses can significantly reduce SAR. Decreasing SAR increases the temperature stability of the tissue being imaged, and reduces the effect of temperature on the measured  $T_1$ . (4) Our method may reduce the influence of chemical exchange on the measured  $T_1$  due to a short TR [37]. (5) Without the need for IR pulses, our approach may reduce the effect of magnetization transfer on the measured  $T_1$ . (6) Different slice profiles for the nominal FAs of 23 and 122° have different influences on the measured  $T_1$  without FA correction. Because FA maps are very sensitive to the slice profiles as shown in Fig. 5, the different slice profiles for the two FAs can give rise to the difference in FA maps. With RF correction, the error resulting from the different slice profiles is taken into account. Finally, though magnetization transfer effects have a small influence on the measured  $T_1$ , they do affect the accuracy of the measured  $T_1$  for multi-slice imaging and this could be an issue of with the variable flip angle

method. Such effects can be reduced if a hard RF pulse is applied to estimate the  $T_1$ . In this work, the acquisition parameters for  $T_1$  measurements were optimized only for GW and WM, and therefore, the measured  $T_1$  of CSF was subject to greater error. It is difficult to optimize this approach for CSF as there can be larger errors in FA maps for the voxels including CSF because the TR used in FA mapping is typically short compared to the  $T_1$  of CSF. These errors give rise to the underestimation of the CSF  $T_1$ .

### 6. Conclusions

In this work, we demonstrate that it is possible to achieve fast and accurate  $T_1$  mapping with the variable flip angle method if FA calibration and correction is used. This approach strongly depends on a precise knowledge of the absolute FA for each voxel. This knowledge can be obtained by calculating relative FA maps and calibration factors in vivo. Experimental results indicate that FA mapping and calibration are sample-dependent, thus, the absolute FA must be measured in vivo. Compared with conventional IR methods, our approach demonstrates high efficiency in obtaining  $T_1$  measurements. In vivo results reveal excellent  $T_1$  images with a short total acquisition time, even taking into account the time required for in vivo RF calibration and field mapping. The novelty of this method lies in the *in vivo* calibration and correction of the FAs, thereby allowing rapid and accurate  $T_1$  mapping at high field for many applications.

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